Hemlock Point Rd.
RUSSELL Tp.

108

LEVEL BOOK

3/3

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julion A. Hall, M. Am. Soc. C. E.

Hemlock Point Road - No. 155
Sections - A B C D
X-Sections - pg - 2-13
Slope Stakes - pg - 14-22

108

J. Gold Jr.
S. Merritt
H. Barton

Hemlock

Sta	+	H.I.	-	Elev.	Remarks
B.M. (Bay Root)	0.55	1144.14		1143.59	Nail in S.E. Corner Small House (W. of Rd.)
0+0					
0+14	(C.I.P.) Culvert				
1+0					
1+55	(C.I.P.) Culvert				Outlet Ditch runs parallel to the rd. 26' ± 25 W. of ℄ (for 75 ft.) & then runs into the same ditch which Culvert Sta 0+14 does)
2+0					
3+0					
T.P.	13.025	1154.855	2.31	1141.83	
4+0					
5+0					
6+0					

Point Rd. (Russell Tp)

Aug. 30, 1923
Fair

West ℄ East

7.3 / 25	6.9 / 19	6.9 / 9	5.9 / 4	5.4	5.0 / 9 (E. Pave)	5.9 / 19 (E. Pave)	5.8 / 21	6.9 / 23	4.4 / 27		
10.4 / 72	8.9 / 48	7.9 / 32	7.2 / 22	7.2 / F.L.	5.8 / 10	5.0	4.6 / 8	4.9 / 28	6.1 / F.L.	5.9 / 32	
		6.9 / 25	6.2 / 14	5.4 / 10	4.8	5.2 / 8	6.1 / 15	5.0 / 18	4.8 / 25		
7.3 / 84	7.0 / 62	6.7 / 42	6.5 / 25	6.4 / F.L.	5.7 / 12	4.8	4.7 / 4	5.6 / 16	6.3 / F.L.	5.8 / 19	5.8 / 25	5.3 / 50
9.2 / 150											
2.6 / Hse	4.8 / 25	5.0 / 19	5.5 / 16	4.8 / 10	4.7	4.5 / 6	5.0 / 12	5.8 / 16	5.4 / 25		
2.9 / 25	3.0 / 19	4.2 / 16	3.8 / 14	3.0 / 5	2.9	3.7 / 13	4.3 / 15	3.7 / 18	3.8 / 25		
		12.0 / 25	12.2 / 20	13.2 / 16	12.3	12.9 / 14	13.3 / 17	12.9 / 20	12.9 / 25		
		10.6 / 25	10.7 / 21	11.4 / 17	10.6	10.5 / 4	11.7 / 17	11.7 / 25			
5.8 / 25	6.0 / 21	8.1 / 17	7.1 / 13	6.5	6.5 / 5	7.9 / 16	8.8 / 17	7.5 / 20	7.6 / 25		

Sta	+	H.I.	-	Elev.	Rems
7+0		1154.855			
T.P.	7.845	1161.79	0.91	1153.945	
8+0					
9+0					
10+0					
11+0					
11+06	Pond on West side of Rd. Ditch running East. (Size of pond rec'd in Topography Notes)				
12+0					
T.P.	7.195	1163.69	5.295	1156.495	
13+0					
14+0					
15+0					

4

West

0.4/25 0.8/20 4.0/15 3.1/13 2.3 2.8/13 3.7/16 2.9/19 3.4/25

4.2/25 4.3/18 7.0/14 6.0/18 5.5 5.4/3 6.9/16 6.2/19 6.6/25

4.3/25 4.5/17 6.0/13 4.9 5.0/4 6.0/15 5.4/18 5.8/25

5.6/25 5.5/17 6.7/14 5.5 6.6/14 5.5/17 5.8/25

8.4/at pond 8.1/14 7.2/10 6.7 7.6/15 7.2/25

8.5/130 7.5/78' 7.6/58 (8.4/15 7.5/11 B. Pond) 6.6 7.6/16 7.9/48 8.5/85 9.3/125 10.6/150

9.6/200'

6.2/25 6.0/16 6.8/13 6.0/9 5.7 6.5/11 7.0/14 6.2/17 6.1/25

7.4/25 7.1/17 7.6/14 6.8/11 6.5 7.9/15 7.0/17 6.9/25

6.1/25 5.8/16 6.2/13 5.8/9 5.2 5.5/9 6.7/16 6.1/19 6.2/25

3.5/25 4.0/21 3.8/17 4.8/14 4.0/9 3.6 4.1/11 4.9/15 4.4/18 4.7/25

3.7/30

East

Sta	+	H. I.	−	Elev.	Remks
		1163.69			
16+0					
B.M.			1.62	1162.07	Nail in E. Root 18" Maple Sta 15+39 40' West of ℄
T.P	4.68	1166.75			
17+0					
T.P.	7.755	1172.76	1.745	1165.005	
18+0					
19+0					
20+0					
21+0					
22+0					
T.P.	0.41	1162.72	10.45	1162.81	
23+0					
24+0					

West ℄ East

1.4/25	1.6/17	2.3/14	1.9/10	1.3	1.3/3	2.0/11	2.7/14	1.7/17	1.8/25
2.5/30	3.0/25	2.1/20	2.5/16	3.5/14	3.3/12	2.4	3.1/11	4.0/15	3.0/18	3.2/25
6.0/25	5.9/21	6.5/16	7.5/14	6.7/6	6.5	6.8/10	7.7/15	6.8/18	7.2/25
4.4/25	4.9/16	6.0/14	5.2/8	4.8	5.5/11	6.3/16	5.6/18	6.0/25	
3.9/25	3.8/22	3.8/16	5.3/14	4.7/7	4.4	4.7/7	5.8/16	6.4/18	5.9/25
3.7/25	4.4/16	6.3/11	5.8/8	5.3	5.6/9	6.7/16	6.4/18	6.8/25	
8.0/25	8.3/18	9.2/14	8.7/10	8.3/6	8.1	8.5/7	9.6/16	8.9/18	9.2/25
3.2/25	3.2/15	4.0/13	3.2/7	2.7	3.1/8	3.9/15	2.9/18	3.2/25	
8.6/25	9.2/17	9.7/14	8.7/10	8.2	8.7/9	10.0/16	9.6/17	10.1/25	

Sta	+	1162.72 H. I.	−	Elev.	Remis
T.P.	1.24	1153.13	10.83	1151.89	
25+0					
B.M.			3.84	1149.29	Spike in N E Root 1-ft 16" Maple Sta 25+80 W.-65 ft. El. 1149.29
26+0					
27+0					
T.P.	0.095	1140.485	12.74	1140.39	
28+0					
29+0					
29+10	C.I.P. Culvert				
30+0					
31+0					
T.P.	2.26	1134.59	8.155	1132.33	
32+0					

West ℄ East

2.0/30 2.9/25 2.4/24 2.9/18 4.1/15 2.8/10 2.4 3.2/11 4.7/15 3.5/18 3.7/25

6.0/25 6.0/19 8.2/16 6.7/13 6.3/6 6.2 6.2/10 8.6/16 6.8/19 7.0/25

10.5/25 10.7/19 12.9/15 11.1/9 10.6 11.0/8 11.8/13 12.6/15 13.5/16 11.0/19 11.4/25

3.2/25 3.4/17 4.2/15 3.3/10 3.0 3.5/10 4.5/16 3.6/18 3.6/25

7.3/25 7.6/16 8.0/15 7.3/13 6.6/6 6.3 6.6/6 8.0/14 8.5/16 7.8/17 8.1/25

6.0/60 7.5/30 8.6/F.L. 7.5/16 6.6/6 6.4 7.2/9 7.9/15 8.5/19 9.3/F.L. 9.4/35 10.9/76 12.2/100

8.3/25 8.8/18 8.0/10 7.5 8.1/9 9.2/16 9.4/25

7.4/25 7.3/20 9.1/16 8.1/7 7.8 8.1/7 8.8/15 8.0/17 8.2/25

2.2/25 2.4/19 4.0/16 3.3/11 2.8 3.6/10 4.0/14 2.8/17 3.1/25

Sta	+	H.I.	-	Elev.	Rem's
		1134.59			
33+0					
34+0					
35+0					
35+67.27					℄ of Larkspur Rd.
36+0					
T.P.	1.585	1124.565	11.61	1122.98	
37+0					
38+0					
39+0					
B.M.			9.80	1114.765	2 Spikes in E. Root 18" Maple W-26' Sta 39+43 El. 1114.765

West				℄				East
3.9/25	4.0/20	5.5/17	4.8/12	4.0	4.5/9	5.4/14	4.2/17	4.3/25
5.5/25	5.5/18	7.2/16	6.1/11	5.3	5.9/10	6.9/14	5.4/17	5.5/25
7.6/25	7.8/18	9.9/15	8.5/12	7.5	8.7/12	9.0/15	7.7/17	7.8/25
		10.2/100	10.2/67	10.0/34	9.8			
11.4/25	11.3/19	13.3/17	12.3/15	11.2/10	10.9	11.3/10	12.1/13	11.1/16	11.1/25
3.5/25	3.6/20	5.6/17	4.1/13	3.6	4.7/11	4.8/14	5.5/15	3.9/17	4.0/25
6.0/25	6.1/18	8.2/15	7.0/13	6.5	7.5/12	8.4/15	7.2/17	7.5/25
8.9/25	8.9/19	12.0/14	10.4/12	9.5	10.3/12	11.5/14	10.0/16	10.3/25

Sept. 3, 1929 Fair

Hemlock Point Rd.

Russell Tp.

S. Gold Jr.
S. Merritt
H. Barton

Sta	+	H.I.	-	Elev.	Rem's	West					℄				East
B.M.	1.735	1116.50		1114.765											
40+0						5.1/25	5.3/17	8.2/15	6.9/13	6.2/7	6.0	5.5/8	8.1/13	5.9/16	6.3/25
40+81.4					℄ of Culvert (12" C.I.P.)	21.0/100	17.5/65	15.5/F.L.	10.4/17	9.8/10	9.3	9.6/15	13.3/19	14.1/F.L.	12.4/65
41+0								15.5/18'	10.2/10		9.5	10.7/14	10.1/17		9.8/25
42+0						10.1/25	9.7/15	10.1/13	9.6/8		9.3	9.4/8	9.8/15	8.8/17	8.6/25
43+0						6.7/25	6.6/16	7.9/14	7.1/9		6.7	7.2/8	7.6/12	5.9/16	5.8/25
T.P.	1.69	1111.79	6.40	1110.1											
44+0						2.0/25	2.1/16	3.5/15	2.7/7		2.2	2.7/7	3.5/13	2.2/16	2.1/25
44+27.27						2.9/25	3.0/17	4.2/14	3.6/11		2.9	3.5/9	4.3/13	2.8/16	2.8/25
B.M.			7.44	1104.35	(34 rec.) Spike in N.E. Root 30" Chestnut W-105' Sta 45+10 El. 1104.34										
45+0						6.9/25	7.0/16	8.3/14	7.6/10		7.1	7.3/7	8.4/14	7.3/16	7.5/25
T.P.	0.84	1101.44	11.19	1100.6											

Notes at 40+81.4 / 41+0: 21.0/100 and 17.5/65 marked "same" with arrow; 15.5/18' marked "F.L. Culvert".

Sta	+	H.I.	-	Elev	Rem's
46+0		1101.44			
47+0					
T.P.	0.345	1090.61	11.175	1090.265	
48+0		Ditch on East Side of Rd.			
49+0					
T.P.	0.34 (.33)	1080.50	10.46	1080.16	
50+0					
B.M.					
50+39.2		℄ of Culvert (12" C.I.P.)			
51+0					
52+0					
T.P.	2.87	1071.525	11.845	1068.655	
53+0					
T.P.	2.31	1064.015	9.82	1061.705	
54+0					

West ℄ East

3.2/25 2.6/16 3.9/13 3.1/12 2.3 3.0/10 4.1/14 2.6/16 2.8/25

8.1/25 8.3/18 9.5/14 8.6/13 7.6 8.2/10 8.9/13 9.6/14 7.7/17 7.5/25

3.0/25 3.8/17 3.9/14 3.2/13 2.8/8 2.2 2.6/9 3.6/14 4.5/15 2.4/17 2.5/21 3.1/25 (Ditch)

7.6/25 7.7/16 8.8/18 8.3/11 7.7 8.4/12 9.2/15 9.9/16 7.3/19 7.1/25

5.0/25 6.0/21 6.4/15 5.6/12 4.8/9 4.1 4.3/10 5.1/14 6.4/16 5.8/17 3.8/19 2.9/25

13.5/69 12.1/48 11.6/38 10.5/F.L 8.3/14 6.8/7 6.2 6.1/5 7.6/17 8.0/21 9.0/F.L 8.3/28

12.6/27 11.8/23 8.4/12 7.1 7.3/7 8.6/17 5.6/23 5.6/25

8.3/25 8.1/25 12.0/15 10.9/8 10.3 10.9/12 12.2/15 9.3/21 7.6/23 7.7/25

4.6/25 4.5/22 9.1/15 8.3/14 7.5/7 7.1 7.3/6 8.3/13 8.9/14 4.6/22 4.5/25

2.6/25 2.4/21 7.2/15 8.4/13 7.3/11 6.6/7 6.4 6.7/6 7.4/12 8.7/14 7.6/15 3.3/25 3.5/25

Sta	+	H. I.	−	Elev.	Remarks
		1064.015			
T.P.	0.905	1056.37	8.55	1055.465	
55+0					
T.P	0.885	1045.02	12.235	1044.135	
55+79.5					℄ of culvert (15" C.I.P.)
					→ Readings taken along the ℄ culvert
					Outlet ditch (west side of Rd) runs parallel with the rd. to a culvert at Sta 57+13
55+83					
56+0					
T.P.	0.28	1033.57	11.73	1033.29	
B.M.			4.79	1028.78	Bent spike in S. side of 14" Maple W-24' Sta 57+72 El. 1028.78
57+0		End of High Bank on East side of Rd.			

West				℄				East
3.1/30	3.1/25	9.4/13	7.9/12	7.4/6	7.1	7.4/6	8.5/12	9.5/13	3.8/21	4.0/25
13.5/27	12.3/FL.	11.1/22	9.9/21	4.8/16	3.5	4.1/17	7.7/F.L.	6.6/26		
6.9/29	8.1/25	9.0/21	4.4/11	3.9	4.1/6	5.2/15	1.9/25	0.3/30		
13.2/30	15.8/25	13.0/19	6.5/10	5.6	5.7/6	6.2/14	5.6/17	0.3/25	+ 0.7/30	
8.2/28	11.4/23	12.1/16	4.1/3	2.7	3.5/3	4.1/12	7.5/19	4.5/20	2.8/25	

Sept 4, 1929 Hemlock Point Rd

Fair Russell TP.

S. Gold Jr.
S. Merritt
H. Barton

Sta	+	H.I.	-	Elev.	Rem's	West	℄	East
B.M.	0.045	1028.825		1028.78	Bent Spike in S. Side of 14" Maple W. 24' Sta 57+72			
57+13	℄ of Culvert (Hillside) readings along ℄ of culvert Outlet Ditch runs into the Creek 70' East of ℄					8.3/F.L. 4.7/19 0.2/6	0.0	0.0/4 1.0/12 6.1/21 11.3/F.L. 12.1/40 13.0/65
57+48	℄ of a 46' Drive (West of Rd.) (Railing on W. side of Rd Ends at Sta 57+25 & begins again at Sta. 57+71)					0.0/29 1.0/23 2.9/12	2.5	2.4/3 3.1/10 9.3/24 10.0/30
58+0						7.5/25 8.1/23 10.9/15 7.0/7	6.7	6.6/2 7.3/11 15.0/25 15.2/30
T.P.	1.97	1018.775	12.02	1016.805				
59+0						9.0/34 9.5/29 11.4/22 5.7/11	5.1	5.9/10 11.8/21 12.5/25 13.8 (℄ of Creek 47' off ℄)
T.P. & B.M.	2.71	1014.55	6.935	1011.84 (845 rec.)	X on N.W. Corner E.H.W. Conc. Bridge Sta 59+ El. 1011.845			
59+39	℄ of Concrete Bridge					11.6/71 11.2/58 10.5/34 10.8/F.L. 2.7/18 2.7/16 3.6/16	2.9	3.2/18 2.8/18 2.8/20 10.1/F.L. 10.0/40

Sta	+	H. I.	-	Elev	Rems
		1014.55			
60+0					
61+0					
62+0					
B.M.	6.83	1018.67		1011.84	X on N.W Corner
63+0	Beg. of High Bank on East Side of Rd				
	Note: For Additional readings on Sta's 63+65.79, 64+0				
63+65.79	See Next page.				
64+0					
65+0					
T.P.	10.245	1028.425	0.49	1018.18	

West ℄ East

7.6/24 8.2/21 8.2/18 5.3/11 4.9/7 4.7 4.7/4 7.7/25 7.9/30
7.4/24

6.7/25 6.9/20 5.3/13 4.6/3 4.7 5.3/7 7.8/25 8.0/34 7.0/40

5.4/25 5.4/22 6.8/19 4.2/14 3.4 4.2/13 5.1/16 4.9/26 4.4/31 3.4/34 3.1/43

8.4/32 7.7/25 7.7/21 6.2/13 5.9/6 6.1 7.3/12 7.2/21 6.8/26 6.0/36 4.5/47 1.8/48

9.6/30 8.8/45 6.7/29 5.9/25 5.3/21 4.7/9 5.1 5.4/3 4.8/4 4.6/8 0.5/14
9.9/35

8.8/42 6.4/25 4.7/13 5.0/14 3.9/7 4.2 4.6/5 4.1/10 0.6/17

8.5/33 7.0/25 6.2/20 5.2/9 5.5/6 4.9 4.6/7 5.2/16 4.9/20 2.1/26 0.2/30

Sta	+	H.I.	−	Elev. Rem's
63+65.79		1028.425		
64+0				
T.P.	1.645	1018.40	11.67	1016.755
T.P.	4.585	1018.33	4.655	1013.745
65+53	End of High Bank on East Side of RA			
	* Bank slope uniform. Same as Sta 65 (2:1)			
65+95	℄ of (C.I P) Culvert + Outlet ditch runs into Chagrin River)			
66+0				
66+50				
67+0				

West ℄ East

9.0/15 8.1/18 5.8/20 3.6/27 0.9/34 0.4/35

7.9/23 5.6/25 4.7/28 4.3/29

10.2/34 12.2/26 12.0/24 10.8/38 6.7/14 6.7/12 7.1/11 6.6/10 5.9 5.5/4 5.8/12 6.3/13 5.8/15 4.3/20 3.8/22 1.9/24 +1.2/25 *

13.7/F.L. 10.7/17 10.6/14 8.0/8 7.3 6.9/3 7.5/14 8.1/18 10.8/F.L. 10.4/30

17.6/33 14.2/30 12.4/25 13.1/27 17.2/17 8.0/8 7.3 6.9/5 7.4/14 7.7/18 10.5/19 10.0/32 9.4/39 8.2/40

9.9/35 8.1/30 8.1/25 8.3/23 6.3/18 5.3/4 5.4 6.3/17 7.5/15 4.3/20 5.8/24 8.0/30 6.4/37

8.1/35 5.2/29 5.0/27 5.5/23 4.3/8 4.5 4.9/4 6.1/13 5.5/15 0.8/20 0.6/27

Sta	+	H.I.	−	Elev.	Rem.
		1018.33			
68+0					
T.P.	5.595	1019.38	4.545	1013.785	
69+0					
69+02.5		℄ of C.I.P. Culvert			
69+16.84		S. Edge of Mac Pave I.C.H. #33			
69+85.84		℄ of Pave I.C.H. #33			
B.M.			8.795	1010.585	X on E. end S Wing wall East End of Bridge over Chagrin River
			6.51	1012.87	El. 1010.57
					X on N.W. Corner L Wing on West Abutment El. 1012.87

West ℄ East

20 83 6.2 5.8 5.9 4.4 4.2 5.7 3.7 2.4 2.0
44 36 30 25 21 8 17 21 34 40
9.5
47

10.3 9.3 8.1 5.8 5.1 4.7 5.0 5.3 6.7 7.1 7.0 6.6
37 25 17 12 6 8 14 17 21 28 41

11.6 10.3 9.8 9.2 5.6 5.2 4.6 5.2 5.5 7.2 6.9
49 35 24 F.L. 13 8 11 16 F.L. 27

5.90 4.40 2.72
25 25

5.63 4.12 2.50
25 25

Hemlock [illegible] (SLOPE STAKES)

May 27 '30

S. Gold Jr.
S. Merritt
H. Barton
Fair

Sta	+	H.I.	−	Elev.	[illegible]	West	℄ Elevation	East
B.M.	1.06	1144.65		1143.59	Nail in S.E. Corner Small Hse El 1143.59			
0+0						F. 1.5 / 21.5'	1138.70	
0+50						F. 1.0 / 22.9'	1138.90	
0+78							39.01	C. 1.5' / 25.0'
1+0						F. 1.5' / 21.4'	1139.10	Gr. / 23.9'
1+50						F. 1.0' / 21.8'	1139.45	F. 1.0' / 22.3'
2+0						F. 1.0' / 22.4'	1140.10	F. 1.5' / 21.5'
2+50						F. 0.5 / 22.9'	1140.90	F. 1.0 / 22'
3+0						F. 0.5' / 22.9'	1141.70	F. 1.0 / 22'
3+50						F. 0.5' / 23.1'	1142.50	F. 1.0 / 22'
T.P.	8.32	1150.32	2.65	1142.00				
4+0						F. 0.5' / 22.9'	1143.30	F. 1.5 / 21.5'

Sta	+	H.I.	−	Elev	Rem.
		1150.32			
4+50					
5+00					
5+50					
6+00					
T.P.	9.57	1158.77	1.12	1149.20	
6+50					
7+00					
7+50					
T.P.	5.36	1162.06	2.07	1156.70	
8+00					
8+50					

West	℄ Elevation	East
F. 1.0 22'	1144.24	F. 2.0' 20.9'
F. 1.5' 21.2'	1145.45	F. 2.0' 20.4'
F. 1.0 22.4'	1146.94	F. 1.5' 21.1'
C. 0.5 24.0'	1148.70	F. 1.0' 21.8
C. 1.0' 25.3'	1150.60	F. 1.0' 22.3'
C. 2.0' 26.2'	1152.50	F 0.5' 22.7'
C. 2.5' 27.1'	1154.19	Gr. 23.5'
C. 2.0' 26.8'	1155.45	Gr. 23.7'
C. 1.0 25.1'	1156.79	F. 0.5' 23.3'

Sta	+	H.I.	-	Elev.	Rem's
		1162.06			
9+00					
10+00					
T.P.	5.76	1161.89	5.93	1156.13	
11+00	No	Stake	Set on	West	Side
12+00					
13+00					
14+00					
T.P.	5.95	1164.03	3.81	1158.08	
15+00					
B.M.	4.90	1166.97	1.96	1162.07	
16+00					
17+00					
T.P.	9.31	1173.22	3.06	1163.91	

West	℄ Elevation	East
C. 1.0 24.9'	1156.70	F. 0.5 23.1'
F. 1.0 22.6'	1157.10	F. 1.0 22.4'
	1157.50	F. 3.0 21.3'
F. 2.0 20.5'	1157.90	F. 2.0 20.3'
F. 2.0' 21.3'	1158.30	F. 1.5 21.3'
F. 1.0 21.9'	1159.03	F. 1.5' 21.5'
G.R. 23.3'	1160.40	F. 1.0 22.1'
C. 0.5 24.3'	1161.10	G.R. 23.5'
G.R. 24.0'	1163.80	G.R. 23.5'

Sta	+	H.I.	−	Elev.	Remarks
		1173.22			
18+00					
19+00					
20+00					
21+00					
T.P.	2.53	1168.64	7.11	1166.11	
22+00					
T.P.	0.08	1158.48	10.24	1158.40	
23+00					
B.M.	5.79	1155.03	9.24	1149.24	B.M.
24+00					
25+00					
26+00					
T.P.	0.25	1146.75	8.53	1146.50	

West	℄ Elevations	East
C. 1.0' / 25.7'	1165.50	C. 0.5' / 24.1'
C. 1.0' / 25.5	1167.20	GR. / 23.5'
C. 1.0 / 25.3'	1167.90	F. 0.5 / 22.7'
C. 1.5' / 27.5'	1166.60	F. 0.5 / 23.1'
C. 1.0 / 25.1'	1164.30	F. 0.5 / 22.9'
F. 2.0' / 20.7'	1161.45	F. 1.5' / 21.1'
F. 3.5 / 22.7'	1157.50	F. 5.0' / 24.5'
F. 2.5' / 20.3'	1153.00	F. 3.5 / 22.1'
F. 1.5' / 21.6'	1148.50	F. 2.0 / 20.4'

Sta	+	H.I.	−	Elev.	Rem's
		1146.75			
27+0					
28+0					
T.P.	2.39	1137.665	11.475	1135.275	
29+0					
30+0					
31+0					
32+0					
T.P.	1.27	1133.405	5.53	1132.135	
33+0					
34+0					
35+0					

West	℄ Elevation	East
F. 1.5' / 21.5'	1144.0	F. 2.0 / 20.7'
F. 2.5' / 20.4'	1139.50	F. 2.5 / 20.0'
F. 2.5' / 19.9'	1135.35	F. 3.0' / 20.1'
F. 1.5 / 21.3'	1133.65	F. 2.5' / 20.3'
C. 0.5 / 24.3'	1132.65	F. 0.5 / 23.3'
C. 0.5 / 24.7'	1131.65	G.R. / 23.5'
G.R. / 23.7'	1130.65	F. 0.5' / 23.2'
F. 0.5' / 23.3'	1129.09	G.R. / 23.7'
C. 0.5' / 24.2'	1126.40	C. 0.5 / 24.3'

Sta	+	H.I.	-	Elev.	Cut
		1133.405			
36+0					
T.P.	1.62	1124.775	10.25	1123.155	
37+0					
38+0					
39+0					
T.P.	2.40	1116.155	11.02	1113.755	
40+0					
B.M.	1.56	1116.29	1.425	1114.73	
41+0					
42+0					
T.P.	6.885	1115.19	7.985	1108.305	
43+0					
44+0					

West	Elev.	East
Gr. 23.6'	1123.15	C. 0.5' 24.1'
C. 1.0' 24.9'	1120.11	C. 0.5' 24.3'
C. 1.0 25.1'	1117.50	F. 0.5' 23.1'
C. 0.5' 24.9'	1114.70	F. 0.5' 23.0'
Gr. 24.1'	1111.10	F. 0.5' 22.7'
F. 7.5' 29.9'	1108.40	F. 2.0' 20.7'
F. 1.5 21.3'	1108.30	Gr. 23.0'
C. 0.5' 24.5'	1109.50	C. 1.0' 25.5'
C. 1.0 24.9'	1109.05	C. 1.0' 25.0

Sta	+	H.I.	−	Elev.	Rems
45+0		1115.19			
T.P.	1.28	1106.07	10.40	1104.79	
46+0					
B.M.			1.715	1104.355	
47+0					
T.P.	0.65	1094.63	12.09	1093.98	
48+0					
49+0					
T.P.	0.0075	1087.795	11.86	1082.77	
50+0					
B.M.					
51+0					
T.P.	1.93	1076.815	7.910	1074.885	
52+0					
53+0					
T.P.	0.65	1067.725	9.74	1067.075	
54+0					

West	℄ Elev.	East
F. 0.5 22.7'	1105.30	F. 0.5 22.7'
F. 1.5' 21.9'	1099.90	F. 1.0' 22.0'
F. 1.5 21.7'	1094.50	F. 0.5' 23.0'
F. 1.5' 21.3'	1089.03	F. 1.5 22.4'
F. 0.5' 23.0'	1083.43	GL. 23.7'
F. 4.0 21.5'	1077.76	F. 1.0' 23.0'
F. 4.5 22.7'	1073.20	C. 1.5 26.0'
C. 2.0' 27.3'	1069.90	C. 3.0' 28.1'
C. 2.0' 26.5'	1065.08	C. 2.0' 26.7'
C. 4.0' 29.1'	1057.60	C. 3.0' 28'

Sta	+	1067.725 H.I. -	Elev	Remarks
T.P. 55+0	0.925	1056.105	12.545	1055.18
56+0				
T.P. 57+0	1.43	1045.115	12.42	1043.685
T.P. 58+0	0.57	1036.055	9.63	1035.485
B.M. 59+0	7.86	1036.64	7.245	1028.81 (1028.78 adjd)
T.P. 60+0	0.785	1029.565	7.86	1028.78
T.P. 61+0	2.80	1024.255	8.11	1021.455
B.M. & T.P. 62+0	3.435	1015.27 (215)	12.42	1011.835
B.M. 63+0	2.87	1014.71		1011.84
T.P.	8.935	1018.68	4.965	1009.745

West	± Elev.	East
C. 45' / 30.1'	1048.80	C. 3.5' / 29.0'
F. 6.0 / 30.0	1040.00	C. 8.0' / 34.5'
F 6.0 / 27.3'	1031.20	F. 2.0 / 21.5'
F. 1.5 / 21.5'	1022.40	F. 8.5 / 32.0'
F. 6.5 / 28.5'	1014.02	F. 8.5 / 32.0
F. 3.5' / 23.7	1010.44	F 3.5 / 22.5
F. 3.0 / 20.7'	1010.72	F. 4.5 / 25.0
F. 2.5 / 20.3'	1011.65	F. 3.0' / 22.5
F. 2.0 / 21.1'	1013.62	F. 2.0 / 21.0'

Hemlock Point Rd. — Aug. 4, 1930

S. Gold Jr
S Merritt

Sta	+	H.I	-	Elev	Rems	West	℄ Elev.		East
63+65.79		1018.68							C.17.5 / 47.0'
64+0	Slope Less the 1½:1 on E. Side					F.2.0 / 20.7'	1014.81		C.16.0 / 42.0
T.P.	10.15	1028.46	0.37	1018.31					
65+0						F.3.0 / 23.5'	1013.36		C.4.0 / 27.0
T.P.	6.81	1032.01	3.26	1025.20					
+50 Used									
+53						F.5.0 / 28.1'	1011.90		C.9.0 / 34.0'
T.P.	8.71	1016.50		1007.79					
66+0	6' Berm on W. Side					F.5.0 / 30.0	1011.10		F.3.0 / 25.3
66+50						F.2.5 / 28.0	1012.94		F.1.0 / 22.7'
T.P.	8.63	1022.28	2.85	1013.65					
67+0						F.0.5 / 31.1'	1013.51		C.3.0 / 26.7'
+45.84	(P.T.)					F.0.5 / 27.1		C.3.0 / 27.1'	
68+0						F.1.5 / 21.5'	1014.05		C.1.0 / 25.5'
69+0						F.4.0 / 22.1'	1014.59		F.2.0 / 20.1'

28+0
HUB 21 572 H.I. 1140.485 − 3.505 = El. 1136.98
39+0
Hub 21 572 H.I. 1124.565 − 10.055 = El. 1114.51

T.P. 1018.67 − 4.94 = 1013.73

9175
9.09
.08 ✓

8'
.085
.08 ✓

1162.07
+8.09
H.I. 1170.16
− 2.755
T.P. 1167.405
2.810
H.I. 1170.215
− 11.855
T.P. 1158.360
+1.11
H.I. 1159.47
− 7.64
T.P. 1151.83
+2.97
H.I. 1154.80
5.575
1149.225

PLEASE RETURN TO GEAUGA COUNTY ENGINEER COURT HOUSE CHARDON, O. PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE; SIDE SLOPES 1½ TO 1

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.